



ASSESSMENT OF EXCAVATOR ENERGY CONSUMPTION AND CUTTING RESISTANCE BASED ON CUT AND SLICE GEOMETRY AND EXCAVATION VELOCITY

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Abstract: *In present paper we examine the dependence of the energy consumption of the excavator and overburden cutting resistance on the cut and slice geometry and excavator arrow velocity. Data analyzed were collected from the bucket wheel excavator at "Tamnava Eastern Field" that was operating until 2008. Using the multiple linear regression, we provided three separate explicit models for estimation of the energy consumption, linear and areal cutting resistance. Results obtained indicate statistically insignificant effect of starting and final cutting angle, while slice height and width and excavator velocity have negative effect of the energy consumption and cutting resistance. This could be explained by the lower resistance to excavation force along the cutting surface, which is reduced to the residual friction angle ones this force overcomes the shear strength. Results obtained confirm that higher excavation efficiency is obtained for larger slice elements.*

Key words: CUTTING RESISTANCE, ENERGY CONSUMPTION,
SLICE GEOMETRY, CUT GEOMETRY, EXCAVATION VELOCITY

INTRODUCTION

Influence of the cutting geometry on the excavation resistance has been in the focus of previous research. According to Trivan [2021], Zelenski was among the first who suggested that both linear and areal cutting resistance are varying with the change in shape and size of the cut element. According

to Bošković [2016], Wojtkiewitch analyzed cutting resistance as a function of surface and shape of the cut element, on the basis of which a new methodology for determining the specific cutting resistance and length of the cutting edges was developed. Jakovljević [2007] examined the impact of the parameters of the cut element on the linear and areal cutting resistance, for bucket wheel excavators. Jakovljević et al. [2010] investigated the effect of slice thickness and width on the specific excavation resistance, along the total slice cross-section area and along the total length of bucket cutting edges, for open pits Tamnava West field and Drmno. Results obtained indicate that specific excavation resistance firstly increases and then it decreases with the increase of slice thickness and width ratio, while excavation resistance in all analyzed cases was significantly greater for smaller slice compared to the optimal slice height. Bošković [2016] analyzed the effect of rock material with the increased strength on the cutting resistance in case of bucket wheel excavator at Gacko surface coal mine. Results obtained indicated that cutting forces is much higher for vertical cut compared with horizontal cut, and that the optimal parameters of the vertical cut for rock material with increased strength are 0.20m for cut thickness and 24 m/min for the rotary velocity of excavator arrow. Miletić et al. [2020] implemented adaptive neuro fuzzy inference system to analyze the bucket wheel drive as a function of the wear of the cutting elements, and conducted analyzes resulted in a reliable predictive model for horizontal frequency. Brinas et al. [2021] established a correlation between the height of the excavated slice and the slewing speed of the boom in order to optimize the drive power of the bucket wheel, in which way the energy efficiency, performance of excavators were improved, reducing, in the same time, operating costs.

Unlike previous research, in present paper we examine the dependence of the maximum energy consumption and cutting resistance (both linear and areal) on the slice geometry (width and height), cut geometry (starting and final cutting angle) and on the rotary velocity of excavation arrow. The aim is to determine the impact of these input parameters on the excavation process, in order to optimize the use of bucket wheel excavators regarding the slice and cut geometry and the velocity of excavation arrow. For this purpose, we implement the method of multiple linear regression, which provided reliable results in our previous research also conducted for bucket wheel excavator [Kostić and Trivan, 2022].

Paper is structured as follows. In Section 2 we describe applied methods and data analyzed. In Section 3 we provide results of our analyzes and corresponding discussion, while final conclusions and given in Section 4.

APPLIED METHODS

In present paper we analyze data from "Tamnava Eastern Field", where bucket wheel excavator SchRs 900 25/6 was in operation until 2008. [Ignjatović, 2003]. In particular, we examined the dependence of maximum energy consumption, linear and areal cutting resistance on the following parameters: starting and final cutting angle, cutting height and depth and perimeter wheel velocity. For this purpose, we use the multiple linear regression analysis, which results in derivation of explicit nonlinear models, whose statistical significance is assessed by ANOVA testing. Data analyzed are presented in Table 1.

Table 1. Overview of the examined parameters and their range of values.

| Analyzed factors | Range of values |
|--|-----------------|
| E_{max} maximum energy consumption (KWh/m ³) | 0.16-0.27 |
| K_{Lmax} maximum linear cutting resistance (N/cm) | 473-833 |
| K_{Fmax} maximum areal cutting resistance (N/cm ²) | 56-104 |
| Ang_s starting cutting angle (°) | -15 - 15 |
| Ang_f final cutting angle (°) | -15 - 15 |
| H cutting height (m) | 3-4 |
| D cutting depth (m) | 0-1 |
| V perimeter wheel velocity (m/min) | 13-24 |

RESULTS

Results of the performed analysis are shown in the following expressions:

$$E_{max} = 1.44 - 0.00015 \cdot Ang_s + 0.0004 \cdot Ang_f - 0.12 \cdot H - 1.21 \cdot D - 0.013 \cdot V \quad (1)$$

$$K_{Lmax} = 4034.67 - 0.68 \cdot Ang_s + 1.49 \cdot Ang_f - 394.1 \cdot H - 3413.55 \cdot D - 22.05 \cdot V \quad (2)$$

$$\ln(K_{Fmax}) = 128.51 - 0.0011 \cdot Ang_s + 0.0021 \cdot Ang_f - 14.48 \cdot H - 144.77 \cdot D - 0.069 \cdot V \quad (3)$$

where E_{max} stands for maximum energy consumption (KWh/m³), K_{Lmax} is the maximum linear cutting resistance (N/cm), K_{Fmax} is the maximum areal cutting resistance (N/cm²), Ang_s and Ang_f are the starting and final cutting angle, H and D are the height of the cut piece and cutting depth (m), while V represents the perimeter wheel velocity (m/min). Physically possible results are obtained for $D < 0.65$ m. Table 2 represents the results of ANOVA tests for Eqs. (1)-(3).

Table 2. Results of ANOVA tests for models (1)-(3)

| Model (1) | | | |
|------------------|-----------------------|----------------|----------------|
| factors | Sum of squares | F value | P value |
| Ang _s | 9.994E-005 | 0.29 | 0.5957 |
| Ang _F | 7.103E-004 | 2.04 | 0.1625 |
| H | 0.018 | 50.90 | < 0.0001 |
| D | 0.016 | 46.32 | < 0.0001 |
| V | 0.027 | 77.77 | < 0.0001 |
| residual | 3.484E-004 | | |
| Lack of fit | 3.338E-004 | 0.86 | 0.6418 |
| Pure error | 3.889E-004 | | |
| Model (2) | | | |
| factors | Sum of squares | F value | P value |
| Ang _s | 2095.82 | 0.67 | 0.4188 |
| Ang _F | 9967.26 | 3.19 | 0.0832 |
| H | 1.852E+005 | 59.19 | < 0.0001 |
| D | 1.285E+005 | 41.07 | < 0.0001 |
| V | 82535.93 | 26.38 | < 0.0001 |
| residual | 1.064E+005 | | |
| Lack of fit | 72202.32 | 0.76 | 0.7215 |
| Pure error | 34186.93 | | |
| Model (3) | | | |
| factors | Sum of squares | F value | P value |
| Ang _s | 5.183E-003 | 0.53 | 0.4721 |
| Ang _F | 0.020 | 2.06 | 0.1600 |
| H | 250.14 | 25517.64 | < 0.0001 |
| D | 231.14 | 23579.37 | < 0.0001 |
| V | 0.80 | 82.11 | < 0.0001 |
| residual | 0.33 | | |
| Lack of fit | 0.23 | 0.83 | 0.6685 |
| Pure error | 0.10 | | |

Statistical analyzes indicated high value of determination coefficient and small values of MSE: R=0.86, MSE=0.017 (for Eq.1), R=0.81, MSE=51.57 (for Eq.2) and R=1.0, MSE=0.091 (for Eq.3). It is clear from normal plots of residuals in Figure 1 that error terms are normally distributed.

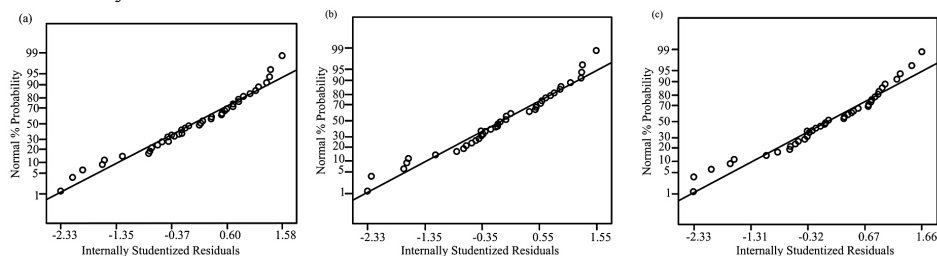


Figure 1. Normal probability plots of residuals for Eq.1 (a), Eq.2(b) and Eq.3 (c).

In all examined cases, analysis showed that only three input factors are significant: height of the cut piece H (m), cutting depth D (m) and the perimeter wheel velocity V (m/min). No significant two-factor interactions were found. Starting and final cutting angle does not have statistically significant effect on the energy consumption nor cutting resistance. As it is seen in Figures 2-4, increase of the cut slice and arrow velocity leads to the decrease of energy consumption and cutting resistance. Such dependence is rather unexpected, since one could assume the increase of cutting resistance and energy consumption with the increase of slice geometry and arrow velocity. However, in this case, decrease of energy consumption and cutting resistance could be explained by the lower cutting resistance for the greater slice once the excavation force overcomes the shear strength along the cutting surface. This is when only the residual friction angle opposes the excavation process. In present case, this residual friction angle is well below 20° , considering the fact that overburden material is mainly composed of small-grained fraction (silt, clay and small-grained sand). These results comply well with the results of Jakovljević et al. [2010].

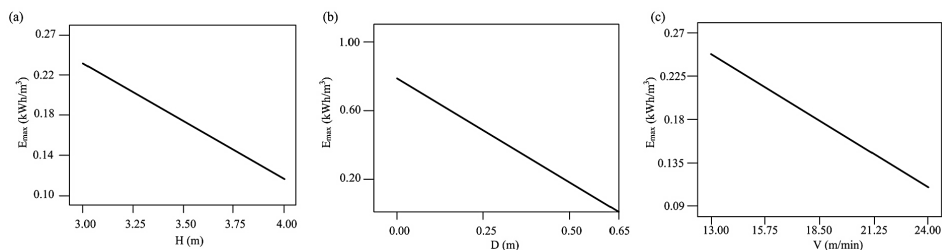


Figure 2. Statistically significant impact of individual controlling factors for maximum energy consumption E_{max} (Eq.1). While a single parameter is varied, other parameters are being held constant at the following values: $H=3.5m$; $D=0.5m$; $V=18.50m/min$.

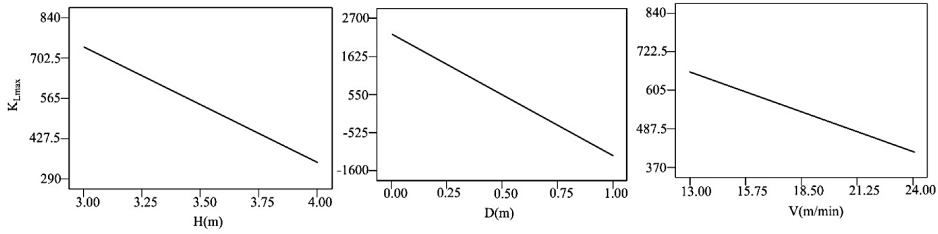


Figure 3. Statistically significant impact of individual controlling factors for linear cutting resistance K_{Lmax} (Eq.2). While a single parameter is varied, other parameters are being held constant at the following values: $H=3.5m$; $D=0.5m$; $V=18.50m/min$.

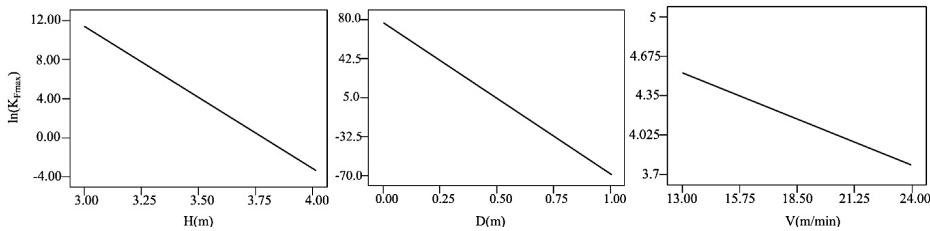


Figure 4. Statistically significant impact of individual controlling factors for areal cutting resistance K_{Fmax} (Eq.3). While a single parameter is varied, other parameters are being held constant at the following values: $H=3.5m$; $D=0.5m$; $V=18.50m/min$.

CONCLUSIONS

In present paper, we present results of the analysis of the effect of cut and slice geometry and excavator arrow velocity on the cutting resistance and energy consumption. Data analyzed were collected for the bucket wheel excavator SchRs 900 25/6 that was in operation at "Tamnava Eastern Field" until 2008. Starting and final cutting angle, slice height and thickness and excavator arrow rotary velocity were examined using multiple linear regression. Results of performed analyzes indicate the following:

- starting and final cutting angle does not have any influence on energy consumption and cutting resistance;
- remaining parameters: slice height and thickness and excavator arrow rotary velocity have a reverse effect on the energy consumption and cutting resistance. In particular, the increase of slice height and thickness and arrow velocity leads to decrease of linear and areal cutting resistance and energy consumption. This could be explained by the lower resistance of the overburden to excavation force, once the shear strength along the potential cutting surface has been overcome.

The results obtained confirm that higher efficiency of the excavation process is obtained with larger cut elements and, consequently, lower arrow velocity, while starting and final cutting angle have no effect on excavation process and can be determined according to the manufacturer's instructions, on the voluntary basis, or can be changed during the excavation process depending on the current needs.

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